

CLAIMS

1. A satellite-based positioning receiver with correction of inter-satellite cross-correlation errors,
5 the receiver comprising a correlation channel C_{ii} of order i per satellite received, with $i=1,2,...N$, N being the number of satellites received (Sat1, Sat2,...SatN), each correlator channel C_{ii} having:
- a carrier correlation path (12), in-phase and
10 quadrature, between the signal received (S_r , B_r) and two respective local quadrature carriers (sine, cosine) generated by an oscillator with digital control of carrier (NCO p);
 - a code correlation path (16) based on the
15 signals I , Q output by the in-phase and quadrature carrier correlation path, with the local codes of the satellite received, provided by a digital generator of local codes;
 - an integrator (20) for providing, for each
20 local code, signals I_c , Q_c at the output of the correlator channel C_{ii} of the satellite received, c designating each of the local codes, characterized in that it comprises, for each correlator channel C_{ii} of the satellite received as many
25 additional correlator channels C_{ix} as additional satellites received with $x=1,2,...N$ and x different from i , and in that the local codes of the satellite received are correlated with the local codes of the other additional satellites C_{ix} .
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2. The satellite-based positioning receiver as claimed in claim 1, characterized in that the local codes of the satellite received for the code correlation path (16, 56) are a punctual code and a
35 delta code, the code correlation path in fact comprising two correlation paths:
- a punctual path (I_P, Q_P),
 - a delta path (I_Δ, Q_Δ).

3. The satellite-based positioning receiver as claimed in claim 1, characterized in that the local codes of the satellite received for the code correlation path (16, 56) are a punctual code, an early code and a late code, and in that the integrator (20) provides signals $(I_P, Q_P, I_A, Q_A, I_R, Q_R)$, the code correlation path comprising three correlation paths:

- an early path (I_A, Q_A) ,
- a punctual path (I_P, Q_P) , and
- 10 - a late path (I_R, Q_R) , the delta path being reconstituted from the early path minus the late path by the formulae:

$$I_\Delta = I_A - I_R$$

$$Q_\Delta = Q_A - Q_R$$

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4. The satellite-based positioning receiver as claimed in either of claims 1 or 2, characterized in that it comprises N reception subsets S_i , each subset S_i of rank i having the correlator channel C_{ii} of the signal of the satellite received of order i and N-1 additional correlator channels $C_{i1}, C_{i2}, \dots, C_{ix}, \dots, C_{iN}$ for the additional satellites received, $x = 1, 2, \dots, N$ and x different from i, each received signal correlator channel C_{ii} being driven by its reception input (E_r) by the signal received (S_r) , each of the additional correlator channels of a subset S_i , receiving respectively, on the one hand, at its received-signal input (E_r) , a local signal S_{lox} resulting from the modulation of the local carrier (F_{lx}) by the punctual local code (C_{px}) of the correlator channel C_{xx} of the satellite received of order x, and on the other hand, at its local carrier and local codes local inputs, the respective local quadrature carriers (F_{li}, F_{qi}) and the local codes $(C_{pi}$ and $\Delta_i)$ of the correlator channel

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(C_{ii}) of the signal received from the satellite of order i.

5. The satellite-based positioning receiver as claimed in claim 4, characterized in that each correlator channel C_{ix} of rank x in the subset S_i , with $x=1,2,\dots,N$, comprises:
- 5 - the in-phase and quadrature carrier correlation path (12) between the signal received and two respective quadrature local carriers (sine, cosine);
 - the code correlation path (16) based on the signals I , Q at the output of the in-phase and
 - 10 quadrature carrier correlation path with the punctual (C_{pi}) and delta (Δ_i) local codes of the satellite of order i ;
 - an integrator (20) for providing signals I_{pix} , $I_{\Delta ix}$, Q_{pix} , $Q_{\Delta ix}$ at the output of the correlator channel,
 - 15 the subset S_i furthermore comprising:
 - an oscillator with digital control of carrier (O_{Pi}) (NCO p) for providing local carriers F_{Ii} , F_{Qi} for the N correlators of the subset S_i considered and a digital generator of local codes (O_{Ci}) for providing
 - 20 the local codes, punctual (C_{pi}) and delta (Δ_i), for the N correlators of the subset S_i considered;
 - a multiplier M_i providing for the other subsets S_x of the receiver a local signal (S_{loi}), resulting from the modulation of the local carrier (F_{Ii}) by the
 - 25 punctual code (C_{pi}) of the subset considered S_i , so as to perform the correlation of the code modulated by the carrier of the satellite considered with the codes modulated by the carriers of the other satellites;
 - a correlation corrector CR_i providing on the
 - 30 basis of the signals I_{pix} , $I_{\Delta ix}$, Q_{pix} , $Q_{\Delta ix}$ at the output of the N correlator channels of the subset considered (S_i), x taking, for these signals I_{pix} , $I_{\Delta ix}$, Q_{pix} , $Q_{\Delta ix}$, the values 1 to N , and signals I_{pxx} , I_{Qxx} output by the received-signal correlator channels C_{xx} of the other
 - 35 subsets S_x , corrected signals I_{pi}' , $I_{\Delta i}'$, Q_{pi}' , $Q_{\Delta i}'$;
 - a carrier discriminator D_{Pi} providing through a carrier loop corrector CB_{Pi} a control signal V_{cpi} for the oscillator with digital control of carrier (NCO p) so as to provide local carriers (F_{Ii} , F_{Qi}) for the N

correlators of the subset S_i considered;

- a code loop discriminator DC_i providing through a code loop corrector CBC_i a control signal V_{cci} for the digital generator of local codes (OC_i) (NCO c) for providing the local codes, punctual (C_{pi}) and delta (Δ_i) for the N correlators of the subset S_i considered.

6. The satellite-based positioning receiver as claimed in one of claims 1 to 5, characterized in that it comprises a first (S_1), a second (S_2) and a third (S_3) reception subset having three correlator channels each for receiving three satellites.

7. The satellite-based positioning receiver as claimed in claim 6, characterized in that the first (S_1), second (S_2), and third subsets (S_3) of the receiver respectively comprise a first (C_{11}), a second (C_{22}) and a third (C_{33}) signal correlator channels driven at their reception input (E_r) by the signal S_r received by the receiver, each subset furthermore comprising:

- in the first subset (S_1), two other additional correlator channels C_{12} and C_{13} driven respectively at their reception input by local signals S_{lo2} , S_{lo3} emanating respectively from a multiplier M_2 and from a multiplier M_3 , the signal S_{lo2} resulting from the modulation of the local carrier F_{12} by the punctual code C_{p_2} of the second satellite and the signal S_{lo3} resulting from the modulation of the local carrier F_{13} by the punctual code C_{p_3} of the third satellite;

- in the second subset (S_2), two other additional correlator channels C_{21} and C_{23} driven respectively at their reception input by local signals S_{lo1} , S_{lo3} emanating respectively from a multiplier M_1 and from a multiplier M_3 , the signal S_{lo1} resulting from the modulation of the local carrier F_{11} by the punctual code C_{p_1} of the first satellite;

- in the third subset (S_3), two other additional correlator channels C_{31} and C_{32} driven at their

reception input by the local signals S_{l01} , S_{l02} emanating respectively from the multipliers $M1$ and $M2$;

each correlator of each of the subsets comprising:

5 - the in-phase and quadrature carrier correlation path (12) between the signal at their reception input and two respective quadrature local carriers (sine, cosine), F_{11}, F_{Q1} for the first subset ($S1$), F_{12}, F_{Q2} for the second ($S2$) and F_{13}, F_{Q3} for the third ($S3$), these
10 carriers being generated respectively, for each of the subsets ($S1, S2$ and $S3$) by a first ($OP1$), a second ($OP2$) and a third ($OP3$) oscillators with digital control of carrier (NCO p);

 - the code correlation path (16) based on the
15 signals I , Q at the output of the in-phase and quadrature carrier correlation path with the local codes, punctual ($Cp1, Cp2, Cp3$) and delta ($\Delta1, \Delta2, \Delta3$) of the satellites respectively of order 1, 2, 3, provided by a digital generator of local codes ($OC1$, $OC2$ and
20 $OC3$) respectively for each subset;

 - an integrator per correlator channel for respectively providing signals $I_{P1x}, I_{\Delta1x}, Q_{P1x}, Q_{\Delta1x}$ at the output of the correlator channel $C1x$; $I_{P2x}, I_{\Delta2x}, Q_{P2x}, Q_{\Delta2x}$ at the output of the correlator channel $C2x$ and
25 $I_{P3x}, I_{\Delta3x}, Q_{P3x}, Q_{\Delta3x}$ at the output of the correlator channel $C3x$, with $x=1, 2, 3$,

each subset of three correlators comprising:

 - a corrector ($Cr1, Cr2, Cr3$) of correlations providing on the basis of the signals $I_{Pix}, I_{\Delta ix}, Q_{Pix}, Q_{\Delta ix}$,
30 with $i=1, 2, 3$, at the output of the N correlator channels of the subset considered ($S1, S2, S3$) and of the signals I_{Pxx}, Q_{Pxx} , at the output of the received-signals correlator channels (of order x) of the other subsets (Sx), of the corrected signals $I_{P1'}, I_{\Delta1'}, Q_{P1'}, Q_{\Delta1'}$ at the
35 output of the first corrector $Cr1$, $I_{P2'}, I_{\Delta2'}, Q_{P2'}, Q_{\Delta2'}$ at the output of the second corrector $Cr2$, $I_{P3'}, I_{\Delta3'}, Q_{P3'}, Q_{\Delta3'}$ at the output of the third corrector $Cr3$, the signals I_{Pxx}, Q_{Pxx} at the output of the received-signal correlator channels, driving the correctors, being the signals

$I_{P22}, I_{P33}, Q_{P22}, Q_{P33}$ for the corrector $Cr1, I_{P11}, I_{P33}, Q_{P11}, Q_{P33}$ for the corrector $Cr2$ and $I_{P11}, I_{P22}, Q_{P11}, Q_{P22}$ for the corrector $Cr3$,

- a carrier discriminator ($DP1, DP2, DP3$)

5 respectively providing through a carrier loop corrector ($CBP1, CBP2, CBP3$) a control signal ($Vcp1, Vcp2, Vcp3$) for the respective oscillator with digital control of carrier ($OP1, OP2, OP3$) (NCO p) so as to provide local carriers F_{11}, F_{Q1} , for the first subset ($S1$), F_{12}, F_{Q2} for

10 the second subset ($S2$) and F_{13}, F_{Q3} for the third subset ($S3$);

- a code loop discriminator ($DC1, DC2, DC3$)

respectively providing through a code loop corrector ($CBC1, CBC2, CBC3$) a respective control signal

15 $Vcc1, Vcc2, Vcc3$ for the digital generator of local codes ($OC1, OC2, OC3$) (NCO c) so as to provide the local codes, punctual and delta ($Cp1, \Delta1$) for the three correlators of the first subset ($S1$), ($Cp2, \Delta2$) for the three correlators of the second subset ($S2$) and ($Cp3, \Delta3$) for

20 the three correlators of the third subset ($S3$).

8. The satellite-based positioning receiver as claimed in either of claims 6 or 7, characterized in that it is configured to perform the following

25 corrections:

for the first satellite $Sat1$:

- on the punctual path:

$$I_{P1}' = I_{P11} - I_{P22} \cdot I_{P12} \cdot 2/T - I_{P33} \cdot I_{P13} \cdot 2/T$$

$$Q_{P1}' = Q_{P11} - I_{P22} \cdot Q_{P12} \cdot 2/T - I_{P33} \cdot Q_{P13} \cdot 2/T$$

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- on the delta path:

$$I_{\Delta1}' = I_{\Delta11} - I_{P22} \cdot I_{\Delta12} \cdot 2/T - I_{P33} \cdot I_{\Delta13} \cdot 2/T$$

$$Q_{\Delta1}' = Q_{\Delta11} - I_{P22} \cdot Q_{\Delta12} \cdot 2/T - I_{P33} \cdot Q_{\Delta13} \cdot 2/T$$

- i.e. in complex notation, with $j^2 = -1$:

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$$I_{P1}' + jQ_{P1}' = I_{P11} + jQ_{P11} - I_{P22} (I_{P12} + jQ_{P12}) \cdot 2/T - I_{P33} (I_{P13} + jQ_{P13}) \cdot 2/T$$

$$I_{\Delta 1}' + jQ_{\Delta 1}' = I_{\Delta 11} + jQ_{\Delta 11} - I_{P22} (I_{\Delta 12} + jQ_{\Delta 12}) \cdot 2/T - I_{P33} (I_{\Delta 13} + jQ_{\Delta 13}) \cdot 2/T$$

with $\frac{T}{2} = \int_0^T (\text{local signal}(t))^2 dt$, T integration period of the

integrator (20).

5 9. The satellite-based positioning receiver as claimed in one of claims 5 to 8, characterized in that in the case where the local carriers are not entirely in phase with the carriers received it is shown that:

for the first satellite Sat1:

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- on the punctual path:

$$I_{P1}' = I_{P11} - (I_{P22} \cdot I_{P12} - Q_{P22} \cdot Q_{P12}) \cdot 2/T - (I_{P33} \cdot I_{P13} - Q_{P33} \cdot Q_{P13}) \cdot 2/T$$

$$Q_{P1}' = Q_{P11} - (I_{P22} \cdot Q_{P12} + Q_{P22} \cdot I_{P12}) \cdot 2/T - (I_{P33} \cdot Q_{P13} + Q_{P33} \cdot I_{P13}) \cdot 2/T$$

- on the delta path:

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$$I_{\Delta 1}' = I_{\Delta 11} - (I_{P22} \cdot I_{\Delta 12} - Q_{P22} \cdot Q_{\Delta 12}) \cdot 2/T - (I_{P33} \cdot I_{\Delta 13} - Q_{P33} \cdot Q_{\Delta 13}) \cdot 2/T$$

$$Q_{\Delta 1}' = Q_{\Delta 11} - (I_{P22} \cdot Q_{\Delta 12} + Q_{P22} \cdot I_{\Delta 12}) \cdot 2/T - (I_{P33} \cdot Q_{\Delta 13} + Q_{P33} \cdot I_{\Delta 13}) \cdot 2/T$$

- i.e. in complex notation, with $j^2 = -1$:

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$$I_{P1}' + jQ_{P1}' = I_{P11} + jQ_{P11} - (I_{P22} + jQ_{P22})(I_{P12} + jQ_{P12})2/T - (I_{P33} + jQ_{P33})(I_{P13} + jQ_{P13})2/T$$

$$I_{\Delta 1}' + jQ_{\Delta 1}' = I_{\Delta 11} + jQ_{\Delta 11} - (I_{P22} + jQ_{P22})(I_{\Delta 12} + jQ_{\Delta 12})2/T - (I_{P33} + jQ_{P33})(I_{\Delta 13} + jQ_{\Delta 13})2/T$$

for the second satellite Sat2:

$$I_{P2}' + jQ_{P2}' = I_{P22} + jQ_{P22} - (I_{P11} + jQ_{P11})(I_{P21} + jQ_{P21})2/T - (I_{P33} + jQ_{P33})(I_{P23} + jQ_{P23})2/T$$

$$I_{\Delta 2}' + jQ_{\Delta 2}' = I_{\Delta 22} + jQ_{\Delta 22} - (I_{P11} + jQ_{P11})(I_{\Delta 21} + jQ_{\Delta 21})2/T - (I_{P33} + jQ_{P33})(I_{\Delta 23} + jQ_{\Delta 23})2/T$$

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and in that for the third satellite Sat3:

$$I_{P3}' + jQ_{P3}' = I_{P33} + jQ_{P33} - (I_{P11} + jQ_{P11})(I_{P31} + jQ_{P31})2/T - (I_{P22} + jQ_{P22})(I_{P32} + jQ_{P32})2/T$$

$$I_{\Delta 3}' + jQ_{\Delta 3}' = I_{\Delta 33} + jQ_{\Delta 33} - (I_{P11} + jQ_{P11})(I_{\Delta 31} + jQ_{\Delta 31})2/T - (I_{P22} + jQ_{P22})(I_{\Delta 32} + jQ_{\Delta 32})2/T$$

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and in that generally:

- on the punctual path:

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$$\begin{aligned} |P_i'| &= |P_{ii}| - \sum_{\text{on } x \text{ different from } i} (|P_{xx}| \cdot |P_{ix}| - Q_{P_{xx}} \cdot Q_{P_{ix}}) \cdot 2/T \\ Q_{P_i'} &= Q_{P_{ii}} - \sum_{\text{on } x \text{ different from } i} (|P_{xx}| \cdot Q_{P_{ix}} + Q_{P_{xx}} \cdot |P_{ix}|) \cdot 2/T \end{aligned}$$

- on the delta path:

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$$\begin{aligned} |_{\Delta i}' &= |_{\Delta ii}| - \sum_{\text{on } x \text{ different from } i} (|P_{xx}| \cdot |_{\Delta ix}| - Q_{P_{xx}} \cdot Q_{_{\Delta ix}}) \cdot 2/T \\ Q_{_{\Delta i}'} &= Q_{_{\Delta ii}} - \sum_{\text{on } x \text{ different from } i} (|P_{xx}| \cdot Q_{_{\Delta ix}} + Q_{P_{xx}} \cdot |_{\Delta ix}|) \cdot 2/T \end{aligned}$$

i.e. in complex notation, with $j^2=-1$:

$$\begin{aligned} |P_i'| + j Q_{P_i'} &= |P_{ii}| + j Q_{P_{ii}} - \sum_{\text{on } x \text{ different from } i} (|P_{xx}| + j Q_{P_{xx}})(|P_{ix}| + j Q_{P_{ix}})2/T \\ |_{\Delta i}' + j Q_{_{\Delta i}'} &= |_{\Delta ii}| + j Q_{_{\Delta ii}} - \sum_{\text{on } x \text{ different from } i} (|P_{xx}| + j Q_{P_{xx}})(|_{\Delta ix}| + j Q_{_{\Delta ix}})2/T \end{aligned}$$

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10. The satellite-based positioning receiver as claimed in one of claims 1 to 5, characterized in that each correlator channel (50) operates with a signal received (Br) in baseband, in the form of two signals I and Q in quadrature.

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11. The satellite-based positioning receiver as claimed in claim 10, characterized in that the baseband correlator channel (50) comprises an in-phase and quadrature correlation path (52) between the baseband signal received, in the form of two signals I and Q in quadrature, and two respective local carriers F_I, F_Q , these local quadrature carriers (sine, cosine) being generated by an oscillator with digital control of carrier (54) (NCO p) of the receiver.

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12. The satellite-based positioning receiver as claimed in claim 11, characterized in that the baseband

receiver comprises N reception subsets for N satellites received, each subset S_i of rank i , with $i=1,2,3,\dots,N$, comprises a correlator channel C_{ii} for a satellite received $S_{at i}$ and $N-1$ additional correlators $C_{i1}, C_{ix}, \dots, C_{iN}$ for the additional satellites $S_{at 1}, S_{at x}, \dots, S_{at N}$, with x different from i , the correlator channel C_{ii} and the additional channels of each subset S_i furthermore comprising:

- a first M_{ii} and a second M_{Qi} multipliers providing for the other subsets of the receiver a first SL_{ii} and a second SL_{Qi} local signals resulting from the modulation of the quadrature signals F_{Qi} and F_{Li} of the local carrier by the punctual code C_{pi} of the subset considered, so as to perform the correlation of the code modulated by the carrier of the satellite considered with the codes modulated by the carrier of the other satellites.

13. The satellite-based positioning receiver as claimed in one of claims 10 to 12, characterized in that it is configured to perform the following corrections:

for the first satellite $S_{at 1}$:

$$\begin{aligned} I_{P1}' + jQ_{P1}' &= I_{P11} + jQ_{P11} - (I_{P22} + jQ_{P22})(I_{P12} + jQ_{P12})/T - (I_{P33} + jQ_{P33})(I_{P13} + jQ_{P13})/T \\ I_{\Delta 1}' + jQ_{\Delta 1}' &= I_{\Delta 11} + jQ_{\Delta 11} - (I_{P22} + jQ_{P22})(I_{\Delta 12} + jQ_{\Delta 12})/T - (I_{P33} + jQ_{P33})(I_{\Delta 13} + jQ_{\Delta 13})/T \end{aligned}$$

14. The satellite-based positioning receiver as claimed in one of claims 3 to 13, characterized in that the delta path is reconstituted at the output of the correlators by the formulae:

$$\begin{aligned} I_{\Delta ix} &= I_{Aix} - I_{Rix} \\ Q_{\Delta ix} &= Q_{Aix} - Q_{Rix} \end{aligned}$$

15. The satellite-based positioning receiver as claimed in one of claims 1 to 13, characterized in

that, to economize on correlators, the cross-correlations are calculated by:

- for the first satellite Sat1, by $(I_P, I_\Delta, Q_P, Q_\Delta)_{12}$
5 and $(I_P, I_\Delta, Q_P, Q_\Delta)_{13}$ in addition to $(I_P, I_\Delta, Q_P, Q_\Delta)_{11}$

$$\begin{aligned} I_{P1}' + jQ_{P1}' &= I_{P11} + jQ_{P11} - (I_{P22} + jQ_{P22})(I_{P12} + jQ_{P12})/T - (I_{P33} + jQ_{P33})(I_{P13} + jQ_{P13})/T \\ I_{\Delta1}' + jQ_{\Delta1}' &= I_{\Delta11} + jQ_{\Delta11} - (I_{P22} + jQ_{P22})(I_{\Delta12} + jQ_{\Delta12})/T - (I_{P33} + jQ_{P33})(I_{\Delta13} + jQ_{\Delta13})/T \end{aligned}$$

- for the second satellite Sat2, by $(I_P, I_\Delta, Q_P, Q_\Delta)_{23}$
10 in addition to $(I_P, I_\Delta, Q_P, Q_\Delta)_{22}$

$$\begin{aligned} I_{P2}' + jQ_{P2}' &= I_{P22} + jQ_{P22} - (I_{P11} + jQ_{P11})(I_{P12} + jQ_{P12})/T - (I_{P33} + jQ_{P33})(I_{P23} + jQ_{P23})/T \\ I_{\Delta2}' + jQ_{\Delta2}' &= I_{\Delta22} + jQ_{\Delta22} - (I_{P11} + jQ_{P11})(I_{\Delta12} + jQ_{\Delta12})/T - (I_{P33} + jQ_{P33})(I_{\Delta23} + jQ_{\Delta23})/T \end{aligned}$$

- and in that for the third satellite Sat3, nothing
15 is calculated in addition to $(I_P, I_\Delta, Q_P, Q_\Delta)_{33}$

$$\begin{aligned} I_{P3}' + jQ_{P3}' &= I_{P33} + jQ_{P33} - (I_{P11} + jQ_{P11})(I_{P13} + jQ_{P13})/T - (I_{P22} + jQ_{P22})(I_{P23} + jQ_{P23})/T \\ I_{\Delta3}' + jQ_{\Delta3}' &= I_{\Delta33} + jQ_{\Delta33} - (I_{P11} + jQ_{P11})(I_{\Delta13} + jQ_{\Delta13})/T - (I_{P22} + jQ_{P22})(I_{\Delta23} + jQ_{\Delta23})/T \end{aligned}$$

and in that by generalizing t, for $x > i$:

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$$\begin{aligned} I_{Pxi} &= + I_{Pix} \\ Q_{Pxi} &= - Q_{Pix} \\ I_{\Delta xi} &= - I_{\Delta ix} \\ Q_{\Delta xi} &= + Q_{\Delta ix} \end{aligned}$$

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- 16. The satellite-based positioning receiver as
claimed in one of claims 1 to 15, characterized in that
in order to improve the accuracy of the estimation of
the complex amplitude of the signals received
30 respectively from the satellites i, the terms I_{Pii} and
 Q_{Pii} in the formulae are replaced with the terms I_{Pi}' and
 Q_{Pi}' , the formulae then becoming:

$$\begin{aligned} I_{Pi}' + j Q_{Pi}' &= I_{Pii} + j Q_{Pii} - \sum_{\text{on } x \text{ different from } i} (I_{Px}' + j Q_{Px}') (I_{Pix} + j Q_{Pix}) / 2T \\ I_{\Delta i}' + j Q_{\Delta i}' &= I_{\Delta ii} + j Q_{\Delta ii} - \sum_{\text{on } x \text{ different from } i} (I_{Px}' + j Q_{Px}') (I_{\Delta ix} + j Q_{\Delta ix}) / 2T \end{aligned}$$

17. The satellite-based positioning receiver as claimed in claim 16, characterized in that, at each iteration of the calculation, the corrected terms I_{Pi}' and Q_{Pi}' of the previous iteration are used, initializing the calculation with uncorrected terms I_{Pii} and Q_{Pii} , after the acquisition and convergence phase:

$$\begin{aligned} (I_{Pi}' + j Q_{Pi}')_n &= (I_{Pii} + j Q_{Pii})_n - \sum_{\text{on } x \text{ different from } i} (I_{Px}' + j Q_{Px}')_{n-1} \cdot (I_{Pix} + j Q_{Pix})_n \cdot 2/T \\ (I_{\Delta i}' + j Q_{\Delta i}')_n &= (I_{\Delta ii} + j Q_{\Delta ii})_n - \sum_{\text{on } x \text{ different from } i} (I_{Px}' + j Q_{Px}')_{n-1} \cdot (I_{\Delta ix} + j Q_{\Delta ix})_n \cdot 2/T \end{aligned}$$

18. The satellite-based positioning receiver as claimed in any one of claims 1 to 17, characterized in that when the signal received is filtered (limited spectrum), the same filtering is applied to the local signals.

19. The satellite-based positioning receiver as claimed in one of claims 1 to 18, characterized in that a first satellite is acquired, without correction, by a conventional open-loop search process, in that on completion of this process we switch to tracking, we deduce therefrom the local signal of this first satellite and we correct the cross-correlations on the other channels in the search phase (in open loop) and in that each time a new satellite is acquired and tracked, we calculate and we apply the cross-correlation corrections in respect of the measurements of all the other satellites already tracked.